

MTC 12L

Using $I_{\alpha}^{(5.1)} = \sum_{\beta} g_{\alpha\beta} V_{\beta}$, $0^{(5.2)} = \sum_{\beta} g_{\alpha\beta} V_{\beta}$,

$= -(g_{31} + g_{32} + g_{34})$

we get from $0 = I_3 = g_{31}V_1 + g_{32}V_2 + g_{33}V_3 + g_{34}V_4$
 $0 = I_4 = g_{41}V_1 + g_{42}V_2 + \cancel{V_3} V_3 + g_{44}V_4$
small \rightarrow
 $- (g_{41} + g_{42} + g_{43})$

$$V_3 = \frac{V_1 g_{31} + V_2 (g_{32} + g_{31} - g_{31})}{g_{31} + g_{32}} = V_2 + (V_1 - V_2) \frac{g_{31}}{g_{31} + g_{32}}$$

$$V_4 = \frac{V_1 g_{41} + V_2 (g_{42} + g_{41} - g_{41})}{g_{41} + g_{42}} = V_2 + (V_1 - V_2) \frac{g_{41}}{g_{41} + g_{42}}$$

$$V_3 - V_4 = (V_1 - V_2) \left[\frac{g_{31}}{g_{31} + g_{32}} - \frac{g_{41}}{g_{41} + g_{42}} \right] = (14.2)$$

1.5.3 Beam splitters

3-lead beam splitter has $3 \times 3 \hat{S}$ -matrix
 \Rightarrow parametrized by 5 real numbers.

fully symmetric beam splitter:
 all diagonal elements must be the same
 " off-diagonal " " " " "

This fixes unitary 3×3 matrix up to 2 phases:

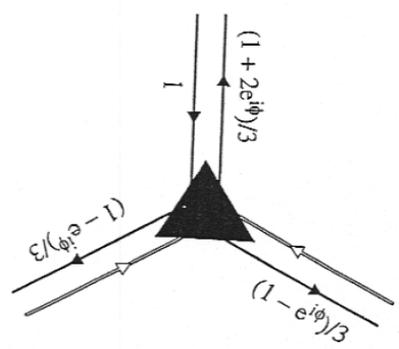
$$\hat{S} = \frac{1}{3} \begin{pmatrix} 1 + 2e^{i\phi} & 1 - e^{i\phi} & 1 - e^{i\phi} \\ 1 - e^{i\phi} & 1 + 2e^{i\phi} & 1 - e^{i\phi} \\ 1 - e^{i\phi} & 1 - e^{i\phi} & 1 + 2e^{i\phi} \end{pmatrix} \quad (1)$$

Reflection in same lead: $R = \frac{1}{3} |1 + 2e^{i\phi}|^2 = \frac{1}{3} (5 + 4 \cos \phi)$, (2)
 Transmission into other lead: $T = \frac{1}{3} |1 - e^{i\phi}|^2 = \frac{1}{3} (2 - 2 \cos \phi)$ (3)

$\phi = 0$: $R = 1$, $T = 0$ \Rightarrow complete reflection (4)
 $\phi = \pi$: $R = 1/9$, $T = 8/9$ \Rightarrow minimal transmission

9.5.2010

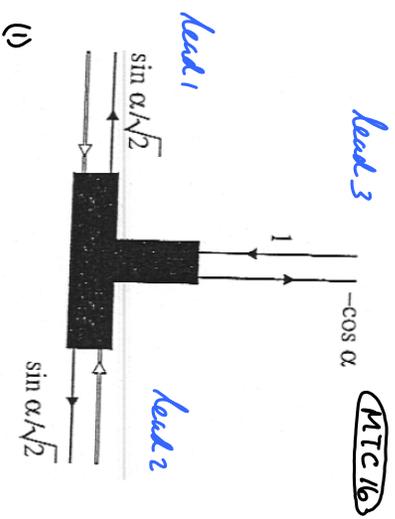
MTC15



T-beam splitter

symmetric w.r.t. lead 1 \leftrightarrow lead 2

$$\hat{S} = \begin{bmatrix} -\sin^2 \alpha/2 & \cos^2 \alpha/2 & \frac{1}{\sqrt{2}} \sin \alpha \\ \cos^2 \alpha/2 & -\sin^2 \alpha/2 & \frac{1}{\sqrt{2}} \sin \alpha \\ \frac{1}{\sqrt{2}} \sin \alpha & \frac{1}{\sqrt{2}} \sin \alpha & -\cos \alpha \end{bmatrix}$$



α parameter coupling between lead 3 and leads 1-2

$\alpha = 0$: 3 is uncoupled, $\begin{cases} 1 \rightarrow 2 \\ 2 \rightarrow 1 \end{cases}$ without any scattering: $\hat{S} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$ (2)

$\alpha = \pi/2$:

$$\hat{S} = \begin{bmatrix} -1/2 & 1/2 & 1/\sqrt{2} \\ 1/2 & -1/2 & 1/\sqrt{2} \\ 1/\sqrt{2} & 1/\sqrt{2} & 0 \end{bmatrix}$$

Ideal beam splitter:
electron incident from 3 is equally divided between 1 & 2
no back-reflection into 3

$$\hat{S} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \\ 0 \end{pmatrix}$$
 (3)

1.54 Coupling statistics device for Multiterminal device:

(MIT 1)

$P(\alpha_1, \alpha_2, \dots, \alpha_N) = \text{prob. that } \alpha \text{ passes from scattering region into lead } \alpha \text{ in time } \Delta t$

$$A(\{X_{\alpha\beta}\}) = \sum_{\alpha_1, \dots, \alpha_N} P(\{N_{\alpha\beta}\}) e^{i(N_{\alpha_1} \alpha_1 + \dots + N_{\alpha_N} \alpha_N)} e$$
 (1)

Current conservation: $\sum_N N_{\alpha_1} = 0 \Rightarrow A$ depends only on differences $X_{\alpha'} - X_{\beta}$

Multiterminal Leitch formula:

$$\ln(A(\{X_{\alpha\beta}\})) = Z_S \Delta t \int \frac{dE}{2\pi t} \text{Tr} \ln \left\{ 1 + \hat{f} + \hat{f} \hat{S} \hat{f}^\dagger \hat{S} \right\}$$
 (2)

leads channels

$$\tilde{S}_{\alpha\beta} = S_{\alpha\beta} e^{i(X_{\alpha'} - X_{\beta})} \quad \tilde{f}_{\alpha\beta} = S_{\alpha\beta} f_{\alpha}(\epsilon) \quad \text{Tr in } \sum_{\alpha} \sum_{\beta}$$
 (3)

Exercise: for 2-terminal device, with

MITC18

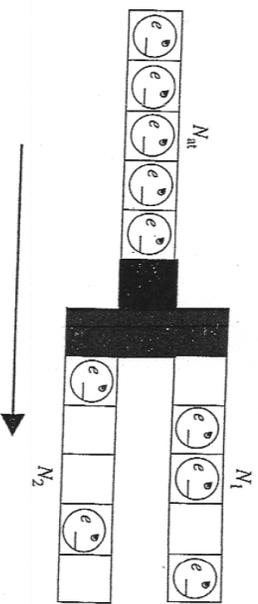
$$\hat{S} = \begin{bmatrix} \sqrt{R} e^{i\theta} & \sqrt{T} e^{i\eta} \\ \sqrt{T} e^{i\eta} & -\sqrt{R} e^{i(2\eta-\theta)} \end{bmatrix}, \quad (\text{see p. SM14}) \quad (1)$$

shows that (17.2) reproduces 2-terminal lead-in formula (EE9.3):

$$\ln N(x) = \int_{\omega} \frac{d\epsilon}{e^2} \sum_p \ln \left\{ 1 + T_p (e^{i\chi} - 1) f_L(1 - f_e) + T_p (e^{-i\chi} - 1) f_e [1 - f_L] \right\} \quad (2)$$

where $\chi = \chi_L - \chi_e$. [Hint: $T_T \log M = \log(\det M)$] (3)

Reflections T-beam splitter:



$$T = 0, \quad V_1, V_2 = 0, \quad V_3 = V > 0.$$

MITC19

$$\Rightarrow N(x_1, x_2, x_3) = \left(\frac{1}{2} e^{i\chi_2} + \frac{1}{2} e^{i\chi_3} \right)^{N_{tot}} e^{-i N_{tot} \chi_3} \quad (1)$$

$N_{tot} = \Delta t \int_{\omega} V/e = \#$ of electrons coming from lead 3 in time Δt .

Distribution of charges $Q_i = e N_i$:

$$P_{N_1, N_2, N_3} = \delta(N_3 + N_{tot}) \delta(N_1 + N_2 - N_3) \binom{N_{tot}}{N_1} \left(\frac{1}{2} \right)^{N_1} \left(\frac{1}{2} \right)^{N_2} \quad (2)$$

current from 3 does not fluctuate: every attempt to inject an electron from 3 is successful (no reflection)

[Every injected electron from 3 arrives either at 1 or 2,

with equal probability of 1/2 each]

\Rightarrow fluctuation of N_1 and N_2 are opposite, since $N_1 + N_2 = N_3 = \text{fixed}$.

MTC203

More generally, it can be shown for arbitrary beam splitters that current conservation at different terminals are negative at $\omega=0$:

$$S_{\alpha\beta}(\omega) = \left\langle \left\langle \hat{I}_{\alpha}(t) \hat{I}_{\beta}(t') + \hat{I}_{\beta}(t') \hat{I}_{\alpha}(t) - 2 \langle \hat{I}_{\alpha}(t) \rangle \langle \hat{I}_{\beta}(t') \rangle \right\rangle_{\omega} \right\rangle$$

$$\langle \rangle_{\omega} = \int dt e^{i\omega t}$$

$$T_{\text{then}} S_{\alpha\beta}(\omega) = \overset{\text{rows}}{-2} \int dE \int_{\Gamma} \left[\underbrace{\sum_{\beta} \hat{a}_{\beta\alpha}^{\dagger} \hat{S}_{\beta\beta}}_{M_{\alpha\beta}} \underbrace{f_{\beta}}_{M_{\alpha\beta}^*} \right] \left[\hat{S}_{\beta\alpha}^{\dagger} S_{\alpha\beta} f_{\beta} \right]$$

< 0 strictly!
 ≥ 0 strictly!

Anticonditions in sense of T-beam splitters reflect that that electrons are fermions: electrons come in one by one, last-in either reflected or transmitted!

1.5.5 Multi-terminal scattering in operator formalism

MTC213

Straightforward generalization of 2-terminal case.

Final result for t -averaged current operator in terminal α :
(compare SFS 9.3)

$$\langle \hat{I}_{\alpha} \rangle_t = -\frac{e}{2\pi t} \left(\frac{2\pi t}{T} \right)^2 \sum_{\mu\sigma} \sum_{\nu\sigma'} \int_{\Gamma} \left[\hat{a}_{\alpha\mu\sigma}^{\dagger} \overset{\text{incoming}}{\hat{a}_{\mu\nu\sigma'}(E)} \hat{a}_{\alpha\nu\sigma}(E) - \overset{\text{outgoing}}{\hat{b}_{\alpha\nu\sigma}(E)} \hat{b}_{\mu\nu\sigma'}(E) \right] \quad (1)$$

$$= -\frac{e}{2\pi t} \left(\frac{2\pi t}{T} \right)^2 \sum_{\mu\sigma} \sum_{\beta\beta'} \sum_{\nu\sigma'} \sum_{\rho\rho'} \hat{a}_{\beta\rho\sigma}^{\dagger}(E) \hat{a}_{\mu\beta'}(E) \times$$

$$\left[\delta_{\alpha\beta} \delta_{\alpha\beta'} \delta_{\mu\nu} \delta_{\nu\rho'} - \delta_{\beta\rho, \mu\nu}^*(E) S_{\alpha\nu, \mu\rho'}(E) \right] \quad (2)$$

$$\text{with } \langle \hat{a}_{\alpha\nu\sigma}^{\dagger}(E) \hat{a}_{\mu\nu\sigma'}(E) \rangle = \delta_{\alpha\nu'} \delta_{\mu\nu} \delta_{\sigma\sigma'} \delta(E-E') \quad (3)$$