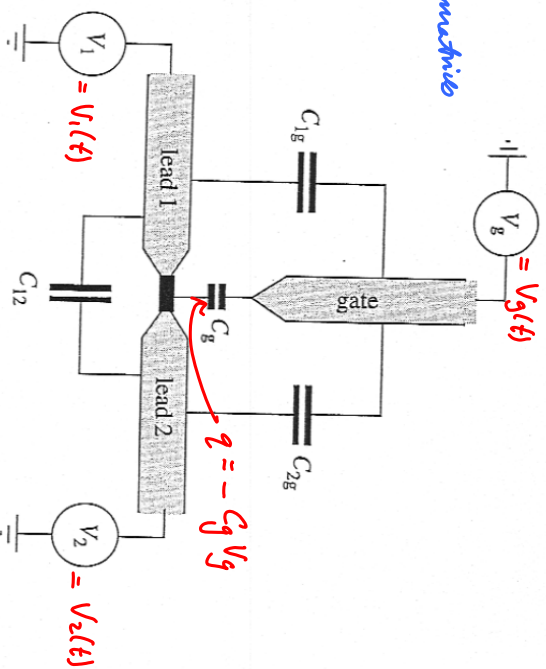


Time-dependent Transport (TDT)

(TDT)

time-dependent gate

⇒ time-dependent scattering matrix



Nanostructure with two leads and a gate. The large external capacitances C_{12} , C_{1g} , and C_{2g} provide paths for ac current, shunting the nanostructure at sufficiently high frequencies.

Displacement currents at finite frequencies: $I_{dis} = \dot{Q} = C \dot{V}$ (TDT2)

Perfect current: $I_{part} = gV$

$I_{dis} \ll I_{part} \Rightarrow C \omega V \ll gV$

⇒ $\omega \ll gC \approx \left(\frac{1}{eR}\right) \cdot 10^{10} \text{ s}^{-1} \approx 10^7 \text{ Hz}$

= small compared to other energy scales
($1K = 20 \text{ GHz} = 2 \times 10^{10} \text{ Hz}$)

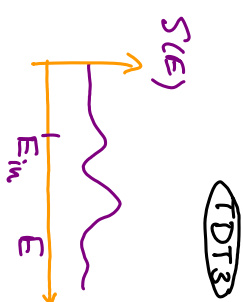
⇒ For ω small enough that displacement currents are negligible, we essentially have $\omega \approx 0$.

Small frequency response:

Scattering approach valid only if $\omega < E_{in}$, where $S(E)$ becomes E -dependent for $E > E_{in}$

Typically: $E_{in} \approx \frac{t_0}{\text{thermal time}}$

[For $\omega > E_{in}$, electrons don't traverse nanosystem, but oscillate back and forth within it.]



(TD13)

Charge accumulation can be ignored only for

$$\omega \lesssim \frac{1}{\tau_{ec}} = \frac{g}{C_g} \gg \frac{g}{C} = \omega_{cap}$$

(since $C_g \ll C$)

[$\omega > \frac{1}{\tau_{ec}}$: capacitive response $\Rightarrow$ currents go via capacitor.]

$$\dot{\rho} + \nabla \cdot \vec{J} = 0 \Rightarrow J_1(\omega) - J_2(\omega) = -i\omega M(\omega)$$

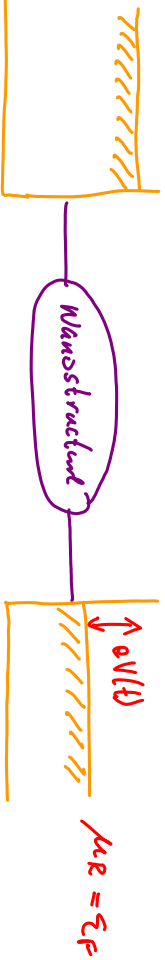
accumulated charge $\rightarrow$

$$\begin{array}{c} \leftarrow U(\omega) \rightarrow \\ J_1(\omega) \quad J_2(\omega) \end{array}$$

$\Rightarrow$ Rather study DC current in presence of time-dependent driving/noise.

1.7.2 Tien-Gordon effect

$$\mu_L = \xi_F + eV(t)$$



(TD14)

$$V(t) = V + \underbrace{\tilde{V} \sin \Omega t}_{\equiv V_{ac}(t)} \quad \text{[spatially uniform]} \quad (1)$$

Claim: $I_{dc}(V) = \sum_k \rho_k \overleftarrow{I}(V + \hbar \Omega t/e)$ $\leftarrow$ I - V curve in absence of modulation, $\tilde{V} = 0$

$$\overleftarrow{I} = J_R^2(e\tilde{V}/\hbar\Omega) \quad (J_R = \text{Bessel function}) \quad (2)$$

Wave function in left lead:

for $V(t) = 0$: $\psi(\vec{r}, t) = e^{-iEt/\hbar} \psi_E(\vec{r})$ (4)

for $V(t) \neq 0$: $\psi(\vec{r}, t) = e^{-iEt/\hbar - ie/\hbar \int dt' V(t')} \psi_E(\vec{r})$ (5)

Suppose $V(t)$ is periodic, eq

(TDTS)

$$V(t) = V + \tilde{V} \sin \Omega t \quad (1)$$

$$\int dt V(t) = Vt - (\tilde{V}/\Omega) \cos \Omega t \quad (2)$$

Fourier series expansion

$$e^{i(e\tilde{V}/\hbar\Omega)\cos\Omega t} = \sum_{l=-\infty}^{\infty} a_l e^{-il\Omega t} \quad (3)$$

Bessel function
more complicated
if $V(t)$ is more compl.
 $a_l = J_l\left(\frac{e\tilde{V}}{\hbar\Omega}\right)$

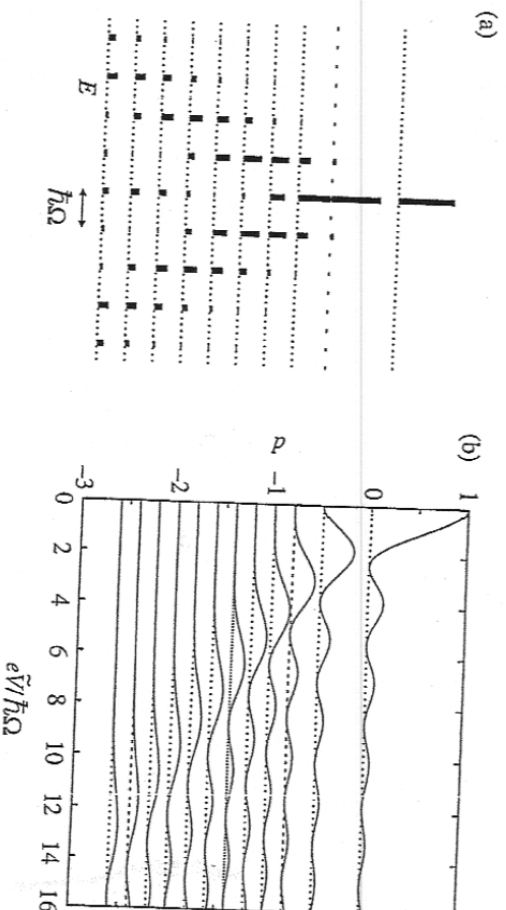
$$\psi(\vec{r}, t) = \sum_{l=-\infty}^{\infty} a_l e^{-i\frac{l}{\hbar}[E + eV + l\hbar\Omega]t} \psi_E(\vec{r}) \quad (4)$$

Energy distribution: $P_E(\varepsilon) = \sum_{l=-\infty}^{\infty} |a_l|^2 \delta(\varepsilon - E - eV - l\hbar\Omega) \quad (5)$

$\equiv P_E$ Probability to be found in l -th component.

Normalization: $\sum_{l=-\infty}^{\infty} P_E = 1 \quad (6)$

(TDTC)



Development of side bands in the presence of ac voltage. (a) Side band weights P_l for $e\tilde{V}/\hbar\Omega$ ranging from 0 to 4.5 with step 0.5. (b) First 12 P_l plotted versus $e\tilde{V}/\hbar\Omega$; oscillations are clearly visible. The curves are offset for clarity.

Now consider tunneling contact, with $\tau_0 \ll 1$.

(TDT7)

Characteristic function:

$$\begin{aligned} \ln \Lambda_{dt}(X) &= 2s \Delta t \int \frac{dE}{2\pi\hbar} \sum_p \ln \{ 1 + \tau_p (e^{iX} - 1) f_L(E) [1 - f_R(E)] \} \\ &\quad + \tau_p (e^{-iX} - 1) f_R(E) [1 - f_L(E)] \} \end{aligned} \quad (1)$$

"Levitov formula" (1996)

$$\ln \Lambda_{dt}(X) = \overset{\tau_0 \ll 1}{\Delta t} \{ (e^{iX} - 1) \Gamma_{Le} + (e^{-iX} - 1) \Gamma_{Re} \} \quad (2)$$

$$\Gamma_{Le} = 2s \int \frac{dE}{2\pi\hbar} \sum_p \tau_p(E) f_L(E) [1 - f_R(E)] \quad (3)$$

$$\Gamma_{Re} = 2s \int \frac{dE}{2\pi\hbar} \sum_p \tau_p(E) f_R(E) [1 - f_L(E)] \quad (3)$$

E-dependence measured relative to τ_0 in R lead $\Rightarrow$

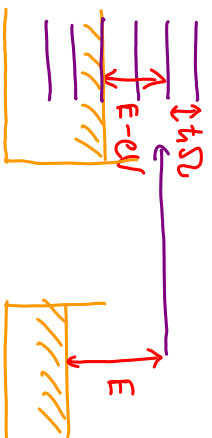
assume making μ_L of left lead does not modify $\tau_p(E)$

(4)

$$\text{Assume: for } \tilde{V}=0: \quad f_R(E) = f_F(E), \quad f_L(E) = f_F(E - eV) \quad (TDT8) \quad (1)$$

$$\text{for } \tilde{V} \neq 0: \quad f_R(E) \rightarrow f_F(E), \quad f_L(E) \rightarrow \sum_p P_e f_F(E - eV - \hbar\Omega p) \equiv \tilde{f}_L(E) \quad (2)$$

Electron moving from R to L can absorb ($R \leftarrow O$) or emit ($O \rightarrow O$) $\hbar$ quanta of energy $\hbar\Omega$, coming from the field.



Tien-Gordon = photon-assisted tunneling.

(CE15.1)

$$\text{Current: } I_{dc} = \frac{e \langle Q \rangle}{\Delta t} = \frac{e}{\Delta t} \left. \frac{\partial \ln \Lambda}{\partial (iX)} \right|_{X=0} \quad (3)$$

$$\begin{aligned} &\overset{(CE15.2)}{=} \frac{e}{\Delta t} \sum_p \int \frac{dE}{e} \tau_p(E) [\tilde{f}_L(E) - f_R(E)] \quad (4) \end{aligned}$$

$$I_{dc} = \sum_p P_e \sum_p \int \frac{d\epsilon}{e} T_p(\epsilon) [f_F(\epsilon - eV - \hbar\Omega/e) - f_F(\epsilon)] \quad \text{TDT 9} \quad (1)$$

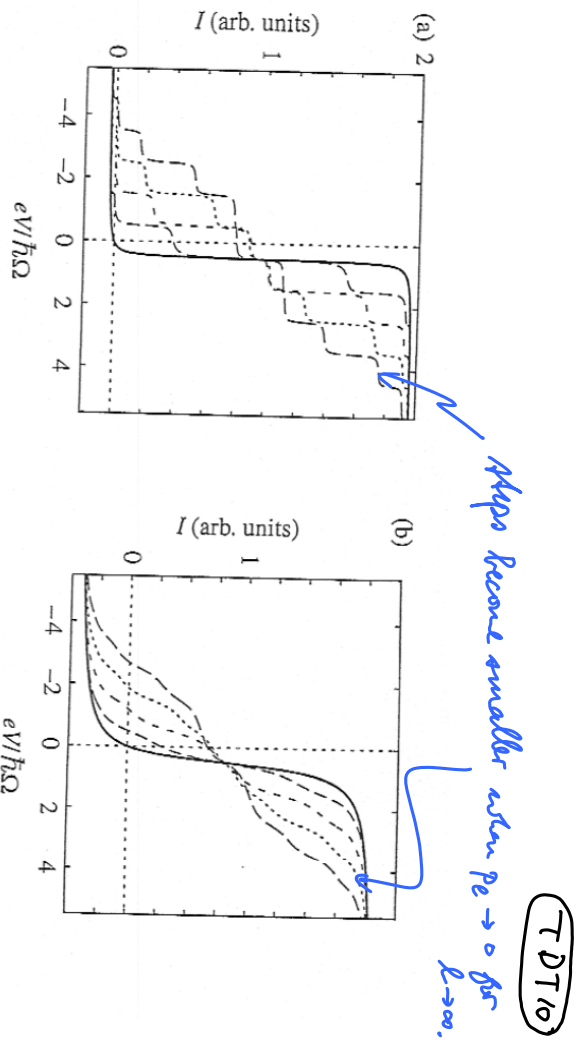
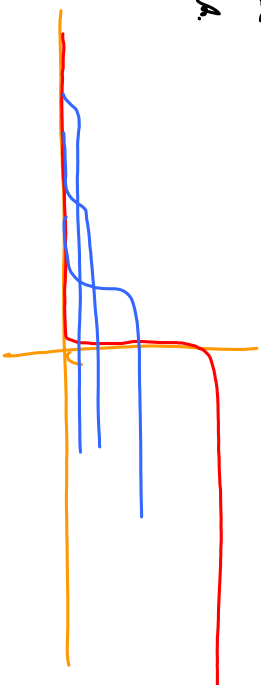
$$= \sum_p P_e I(V + \hbar\Omega/e) \quad \text{constant at DC-bias } V + \hbar\Omega/e \quad (2)$$

Similarly for zero-frequency noise:

$$S_{dc} = \sum_p P_e S(V + \hbar\Omega/e) \quad \text{noise at DC-bias } V + \hbar\Omega/e \quad (3)$$

I_{dc} , S_{dc} are sums of shifted functions with decreasing weights given rise to step functions.

If $I(V)$ is linear $\sim V$,
 as $\sim I_{dc}(V)$ i.e. no steps



Tien-Gordon modification of dc I - V curves (thick solid lines). (a) Sharp step of dc I - V curve at $V_0 = 0.5\hbar\Omega$ is multiplied in the presence of ac voltage to be seen at any $V = V_0 + \hbar\Omega/e$. Subsequent curves correspond to $eV/\hbar\Omega$, ranging from 0 to 4 with step 1. (b) The same curves fit a less sharp step. The peculiarities are barely seen and dc voltage mainly results in overall smoothing of the curve.

$$a_l = \int_0^1 \left(\frac{e\tilde{V}}{\hbar\Omega} \right) = \int_0^1 \tilde{V}(\tilde{V}_\Omega) , \text{ where } \tilde{V}_\Omega = \hbar\Omega/e \quad (1)$$

If $\tilde{V}/\tilde{V}_\Omega < 1$, $a_l \approx 0$ for $l \neq 0$ for photons emitted or absorbed. (2)

If $\tilde{V}/\tilde{V}_\Omega \gg 1$, $\Rightarrow$ many photons, but (3)

modulation slow relative to shift in $V(t) = V + \tilde{V} \sin \Omega t$

$\Rightarrow$ (4.2) reduces to its adiabatic limit, namely time-average over 1 period.

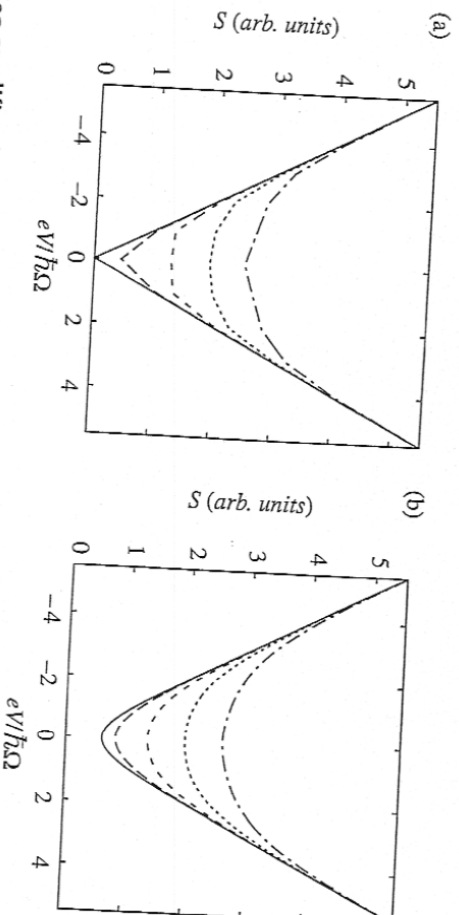
$$I_{dc} = \int_0^{2\pi/\Omega} dt \left(\frac{\Omega}{2\pi} \right) I(V + \tilde{V} \sin \Omega t) \quad (4)$$

Rectification: I_{dc} can be $\neq 0$ even if $V=0$, provided $I(V) \neq \text{odd in } V$.

[for both (2.2) and (11.4)]. Dissipated power $I_{dc}V$ can be $< 0 \Rightarrow$

Power source gains energy (from ac EM-field) when trapping electrons!

(TD7/2)



Tien-Gordon modification of voltage-dependent noise. (a) For $k_B T \rightarrow 0$ the noise curve has a cusp at $V=0$. This cusp is multiplied in the presence of ac voltage. (b) If the cusp is smoothed by the temperature ($k_B T = \hbar\Omega$ is taken), the ac voltage just smooths it further. This results in increased noise at zero dc voltage. The values of $eV/\hbar\Omega$ corresponding to different curves are the same as in Fig. 1.46.

1.7.4 Adiabatic Pumping

(cyclic variation of $\psi(t)$)

(TDT 13)

Charge transported to transport channel j upon $\hat{S} \rightarrow \hat{S} + \delta \hat{S}$:

Ansatz: $\delta \hat{Q}_j = \frac{-ie}{2\pi} (\delta \hat{S} \hat{S}^{\dagger})_j$ (to be motivated below):

or, if $S = S(E)$: $= \frac{-ie}{2\pi} \int dE \left[-\frac{\partial f(E)}{\partial E} \right] (\delta \hat{S}(E) \hat{S}^{\dagger}(E))$: (2)

Consequence: Current induced in terminal α :

$I_{\alpha} = \sum_j \frac{\delta \hat{Q}_j}{\delta t}$ [sum over all channels j in lead α] (3)

$= \frac{ie}{2\pi} \int dE \frac{\partial f(E)}{\partial E} \sum_{\gamma} T_{\gamma} \delta \hat{S}_{\alpha \gamma}(E) \hat{S}_{\gamma \alpha}^{\dagger}(E)$ (4)
 ↑ over all channels

Plausibility arguments for (13.1), (13.2):

(TDT 14)



Change in channel: $\delta Q = \text{ch. density} = e \delta L \int_{-\infty}^{\infty} \frac{dk_x}{2\pi} \underbrace{f(k_x)}_{|k_x| < k_F} = \frac{e k_F \delta L}{\pi}$ (2)

Wavefunction in incident channel: $\psi(x) = e^{-ik_F x} + e^{+ik_F x} e^{i\theta}$ (3)

$\theta \rightarrow \theta + \delta \theta$ implies $L \rightarrow L + \delta L$: $\psi(L) = e^{-ik_F L} [1 + e^{+i2k_F L} e^{i\delta \theta} e^{i\theta}]$ (4)

"size of scatterer changes" $\rightarrow$ "size of channel changes": $= [1 + e^{+i2k_F (L + \delta L)} e^{i\delta \theta} e^{i\theta}]$ (5)

$\delta \theta \equiv 2k_F \delta L$ (6)

$\Rightarrow \delta Q = \frac{e}{2\pi} \delta \theta = -\frac{ie}{2\pi} \delta S S^{\dagger}$ (cf. 13.1) (7)

II: Recover Landauer formula

(TDTr15)

Voltages on lead α : $V_\alpha(t)$ (not small)

$$\Rightarrow \psi_\alpha(t) \xrightarrow{(4.5)} \psi_\alpha(t) e^{i\phi_\alpha}, \quad \phi_\alpha = -\frac{e}{\hbar} \int_t^1 V_\alpha(t') dt' \quad (1)$$

$$\hat{S}_{\alpha\beta} \rightarrow e^{i(\phi_\alpha - \phi_\beta)} \hat{S}_{\alpha\beta} \quad (2)$$

$$\hat{S}_{\alpha\beta} \rightarrow -ie/\hbar (V_\alpha - V_\beta) \hat{S}_{\alpha\beta} \quad (3)$$

$$I_\alpha = \frac{ie}{2\pi} \int dE \frac{\partial f(E)}{\partial E} \sum_\gamma \text{Tr} [\hat{S}_\alpha^\dagger(E) \hat{S}_\gamma(E)] \quad (4)$$

$$= \int dE \underbrace{\left(-\frac{\partial f(E)}{\partial E}\right)}_{=1} \sum_\gamma (-1) \underbrace{g_\alpha \text{Tr} (\hat{S}_{\alpha\gamma} - \hat{S}_{\alpha\gamma}^\dagger)}_{g_{\alpha\gamma}} V_\gamma \quad (5)$$

$$= \sum_\gamma g_\alpha g_\gamma V_\gamma = \text{multiterminal Landauer (MTC 4.4)} \quad (6)$$

Pumpig with two-terminal on-channel conductor:

(TDTr16)

$$\hat{S} = \begin{pmatrix} \sqrt{R} e^{i\theta} & \sqrt{T} e^{i\eta} \\ \sqrt{T} e^{i\eta} & -\sqrt{R} e^{i(\eta-\theta)} \end{pmatrix} \quad \text{for:} \quad \begin{aligned} R(t), T(t) &= 1-R \\ \theta(t), \eta &= \text{fixed.} \\ \delta T &= -\delta R \end{aligned} \quad (1)$$

$$\hat{S}\hat{S}^\dagger = \begin{pmatrix} \sqrt{R} e^{i\theta} \left(\frac{1}{2}\frac{\delta R}{R} + i\delta\theta\right) & \sqrt{T} e^{i\eta} \frac{1}{2}\frac{\delta T}{T} \\ \sqrt{T} e^{i\eta} \frac{1}{2}\frac{\delta T}{T} & -\sqrt{R} e^{i(\eta-\theta)} \left[\frac{1}{2}\frac{\delta R}{R} - i\delta\theta\right] \end{pmatrix} \quad (2)$$

$$\delta Q_L = \frac{-ie}{2\pi} \left(\hat{S}\hat{S}^\dagger \right)_L = \frac{e}{2\pi} R \delta\theta \quad (3)$$

$$\delta Q_R = \frac{-ie}{2\pi} \left(\hat{S}\hat{S}^\dagger \right)_R = -\frac{e}{2\pi} R \delta\theta \quad (4)$$

$\delta\theta = 2\hbar e \delta L$: scatter shifts

$\hat{S}$:



$\delta \leftrightarrow \delta \hat{S}$

$$\delta Q_L = -\delta Q_R$$

Algebra:

$$\begin{bmatrix} \sqrt{R} e^{i\theta} \left(\frac{1}{2} \delta R + i \delta \theta \right) & \sqrt{T} e^{i\gamma} \left(\frac{1}{2} \delta T + i \delta \gamma \right) \\ \sqrt{T} e^{i\gamma} \left(\frac{1}{2} \delta T + i \delta \gamma \right) & -\sqrt{R} e^{i(\gamma-\theta)} \left[\frac{1}{2} \delta R + i(2\delta\gamma - \delta\theta) \right] \end{bmatrix} \cdot \begin{bmatrix} \sqrt{R} e^{-i\theta} & \sqrt{T} e^{-i\gamma} \\ \sqrt{T} e^{i\gamma} & -\sqrt{R} e^{i(\gamma-\theta)} \end{bmatrix}$$

(TDT17)

LC: $\left(\frac{1}{2} \delta R + i \delta \theta R \right) + \left(\frac{1}{2} \delta T + i \delta \gamma T \right) = i \left(\delta \theta R + \delta \gamma T \right)$

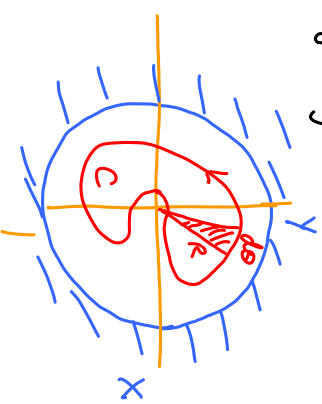
RR: $\left(\frac{1}{2} \delta T + i \delta \gamma T \right) + \left[\frac{1}{2} \delta R + i(2\delta\gamma - \delta\theta)R \right] = -i \left[\delta \theta R + \delta \gamma T - 2 \right] i 2\delta\gamma(1-T)$

(TDT18)

Let $R(t)$ and $\theta(t)$ vary in cyclic fashion, parametrized by

$$X = \sqrt{R} \cos \theta, \quad Y = \sqrt{R} \sin \theta, \quad (1)$$

$$(\text{with } X^2 + Y^2 \leq 1) \quad (2)$$



Charge pumped per period:

$$Q_L^{(U.S)} = \int_0^{\text{Period}} dt \frac{dQ_L}{dt} = \frac{e}{2\pi} \int_0^{\text{Period}} dt R(t) \frac{d\theta}{dt} \quad (3)$$

$$= \frac{e}{2\pi} \oint R d\theta = \frac{e}{\pi} \int_C dX dY = \frac{e}{\pi} A_C \quad (4)$$

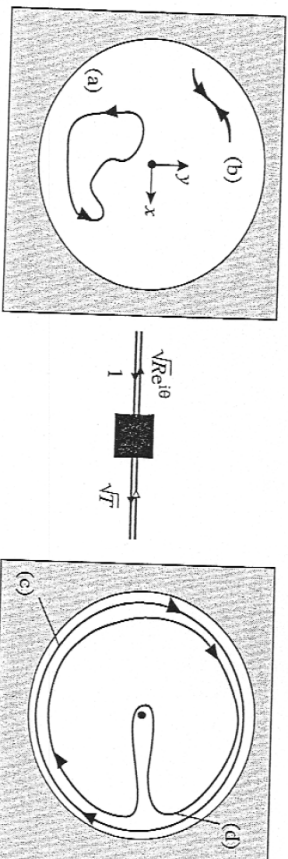
↑ ± area of contour
surfact counter-clockwise / clockwise

Not charge pumped has nice graphical interpretation!

Only contours are allowed for which pump action is cyclic, i.e.

$$\oint_{\partial S} \vec{F} \cdot d\vec{r} = \text{net displacement of scatterer} = 0$$

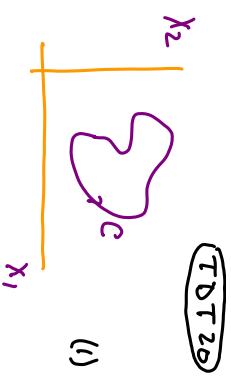
Moreover: enclosed area $\neq 0$ is required.



Different pumping cycles of a one-channel scatterer plotted in convenient coordinates (see the text). The net charge pumped over the period is given by the area enclosed by the closed contour (a) presenting the pumping cycle. The pumping requires variation of two independent parameters: contour (b), corresponding to a one-parameter cycle, encloses no area. Cycle (c) is forbidden because the corresponding contour encloses the origin (the cycle would give rise to a net shift of the scatterer). Cycle (d), which is very similar to cycle (c), is allowed.

General case (multi-terminal)

$$S(t) = S(X_1(t), X_2(t)) \quad (1)$$



$$\text{Transport charge: } \delta Q_j^{(3,1)} = -\frac{ie}{2\pi} \oint \left(\delta \hat{S} \hat{S}^+ \right)_j \quad (2)$$

$$= -\frac{ie}{2\pi} \left[\left(\frac{\partial \hat{S}}{\partial X_1} \hat{S}^+ \right)_j \delta X_1(t) + \left(\frac{\partial \hat{S}}{\partial X_2} \hat{S}^+ \right)_j \delta X_2(t) \right] \quad (3)$$

$$\text{Transport charge per cycle: } Q_j^{\text{cycle}} = \oint \delta Q_j \quad (4)$$

$$\text{Use Green's formula: } \oint_{\partial C} \vec{F} \cdot d\vec{r} = \int dX_1 dX_2 \left(\frac{\partial F_2}{\partial X_1} - \frac{\partial F_1}{\partial X_2} \right) \quad (5)$$

$$-\frac{i}{2} \left[\frac{\partial F_2}{\partial x_1} - \frac{\partial F_1}{\partial x_2} \right]_{j,i} = -\frac{i}{2} \left[\frac{\partial}{\partial x_1} \left(\frac{\partial \tilde{S}}{\partial x_2} \tilde{s}^+ \right)_{j,i} - \frac{\partial}{\partial x_2} \left(\frac{\partial \tilde{S}}{\partial x_1} \tilde{s}^+ \right)_{j,i} \right] \quad (\text{TDT21}) \quad (1)$$

$$= -\frac{i}{2} \left[\left(\frac{\partial \tilde{S}}{\partial x_2} \frac{\partial \tilde{s}^+}{\partial x_1} \right)_{j,i} - \left(\frac{\partial \tilde{S}}{\partial x_1} \frac{\partial \tilde{s}^+}{\partial x_2} \right)_{j,i} \right] \quad (2)$$

$$= -\int_{\mathcal{C}} \left(\frac{\partial \tilde{S}}{\partial x_1} \frac{\partial \tilde{S}}{\partial x_2} \right)_{j,i} = K_j(x_1, x_2) \quad (3)$$

$$Q_{\text{cycle}}^{(2014)} = \frac{e}{\pi} \int_{\mathcal{C}} dx_1 dx_2 K_j(x_1, x_2) \quad (\text{Brouwer formula}) \quad (4)$$

↪ area enclosed by pumping loop.

NICE GEOMETRIC INTERPRETATION !!